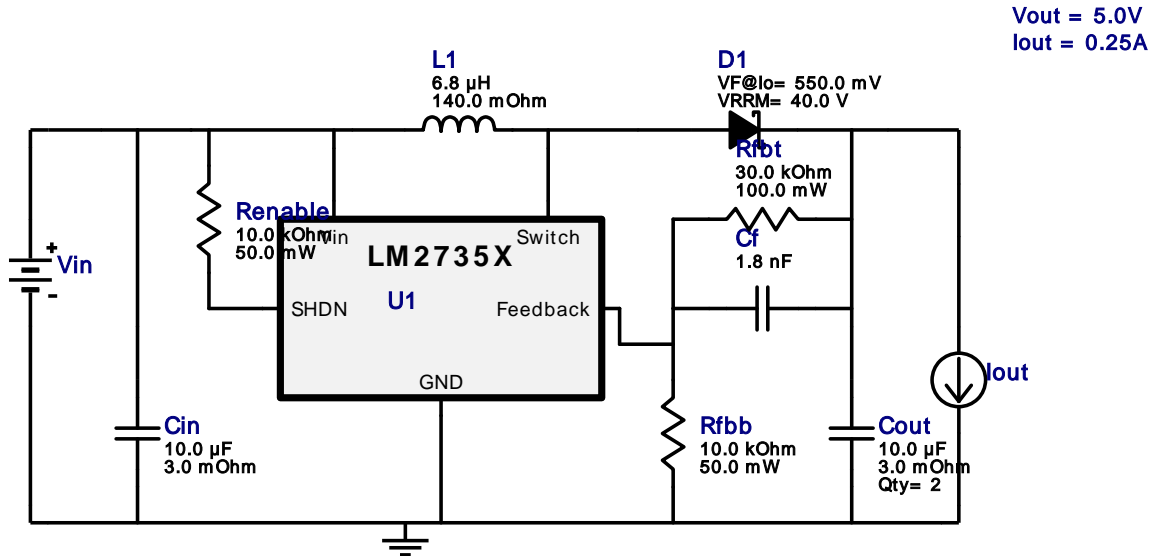
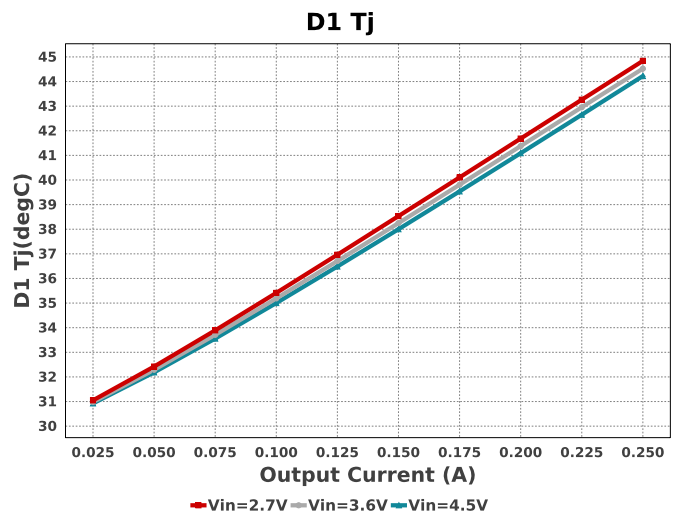
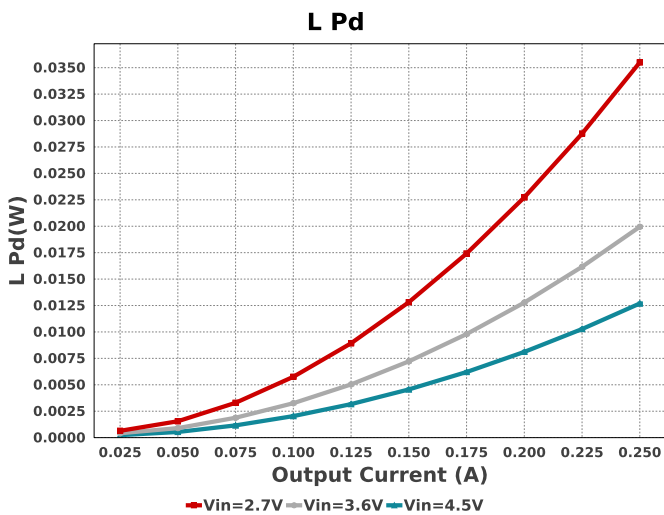
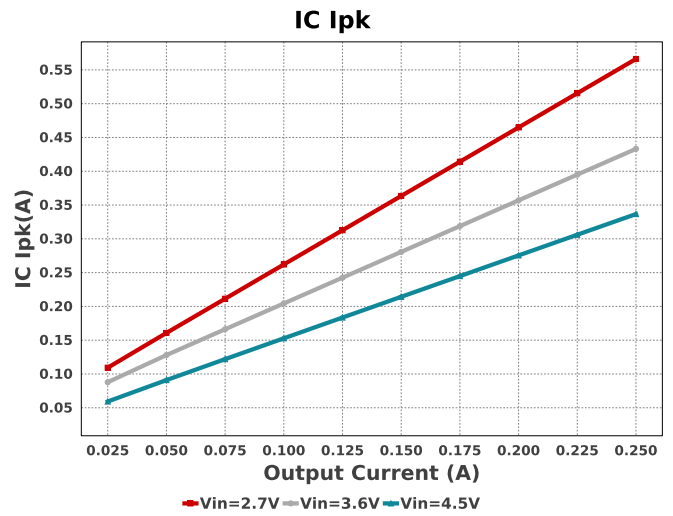
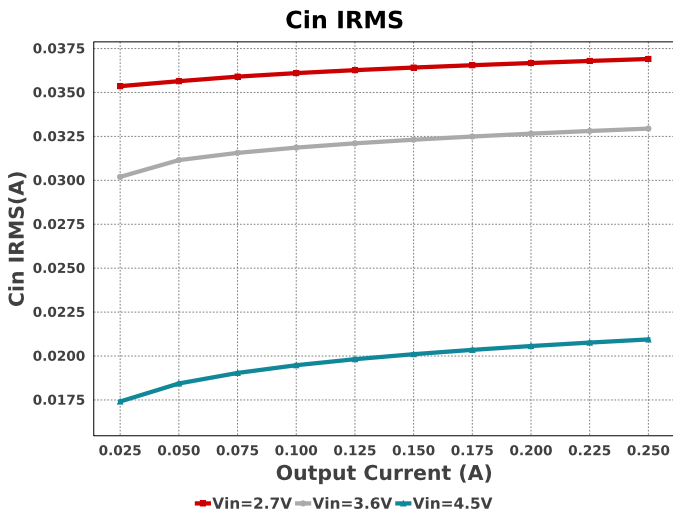
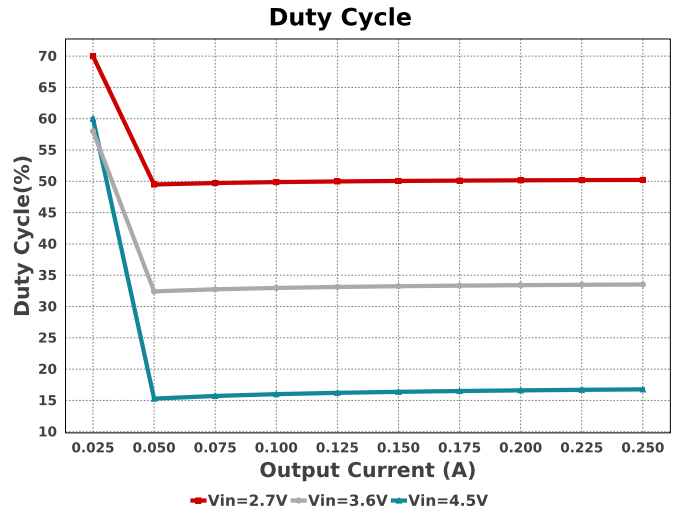
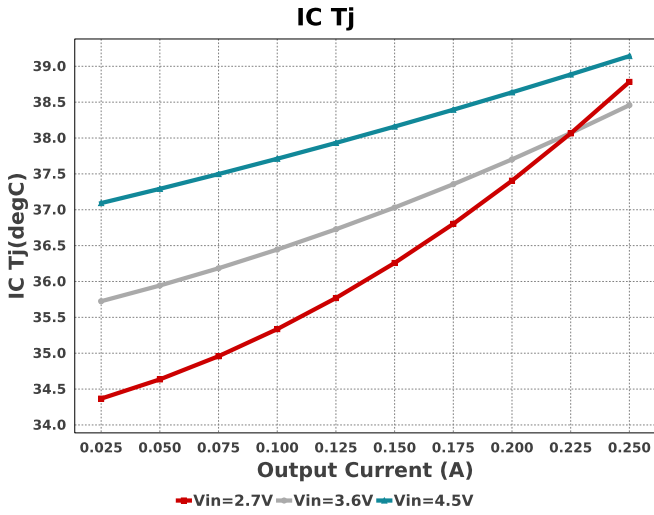
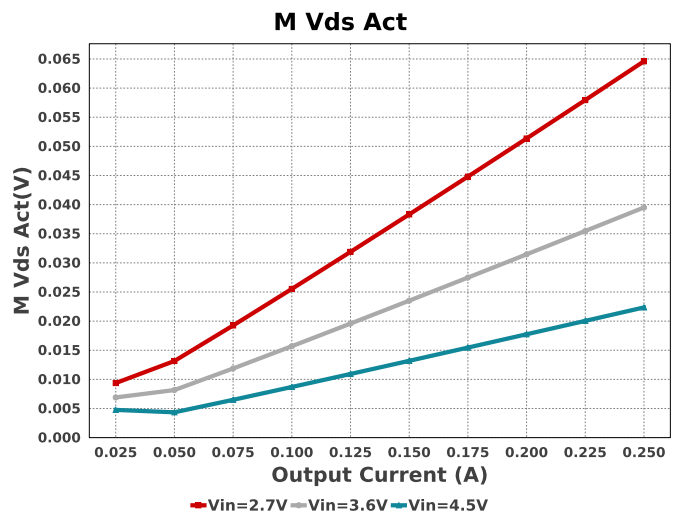
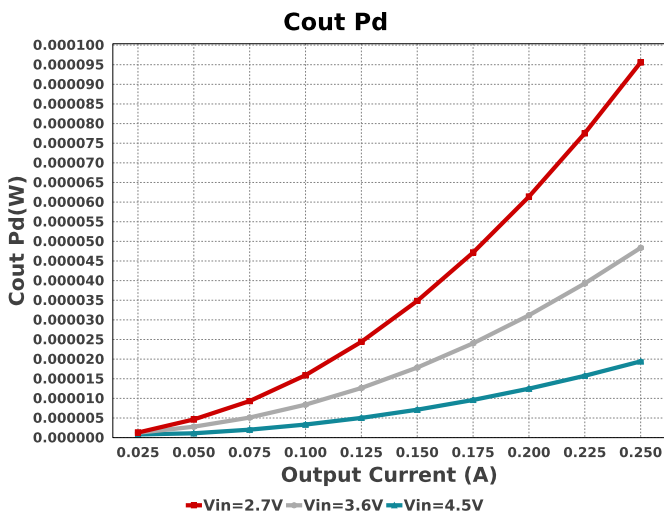
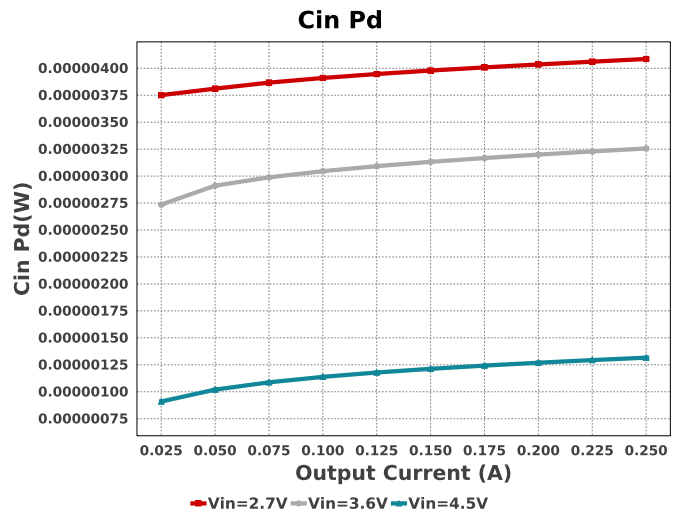
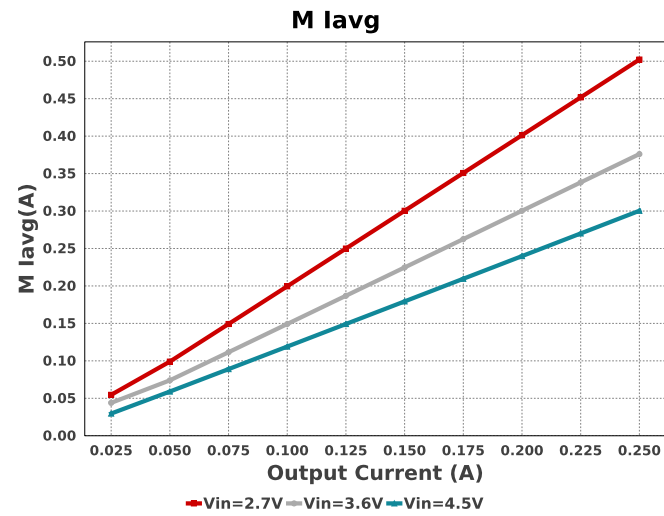
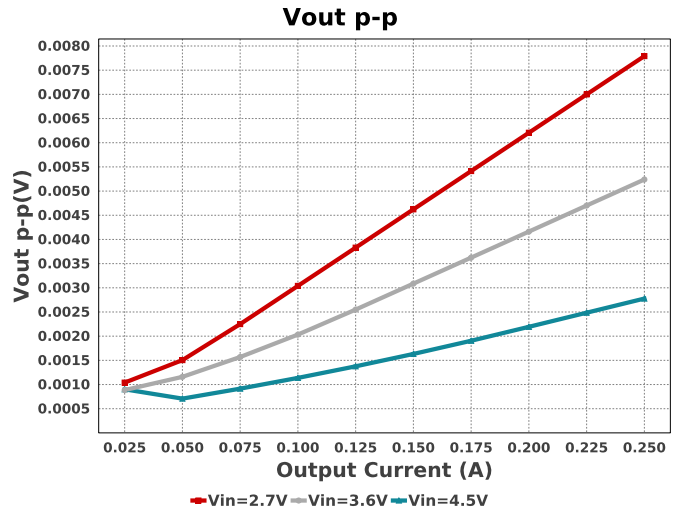
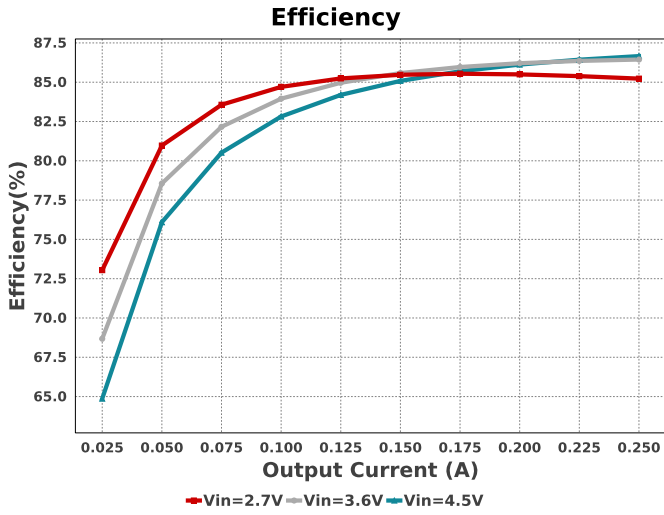


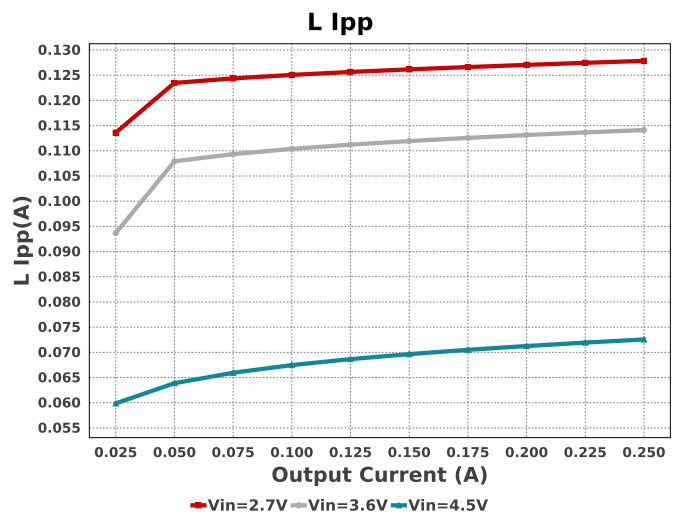
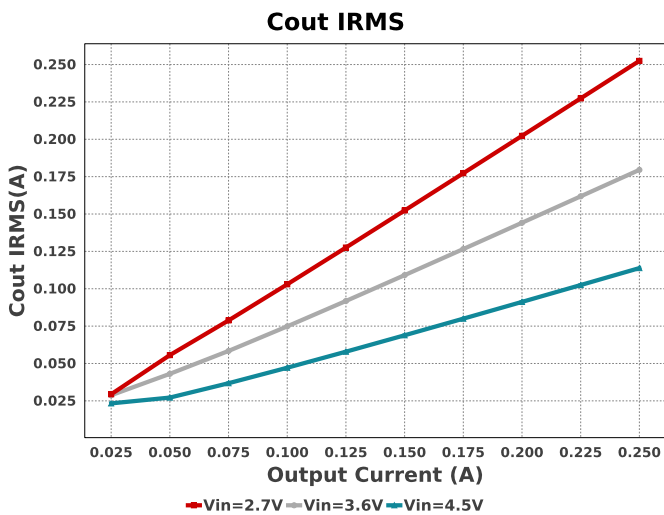
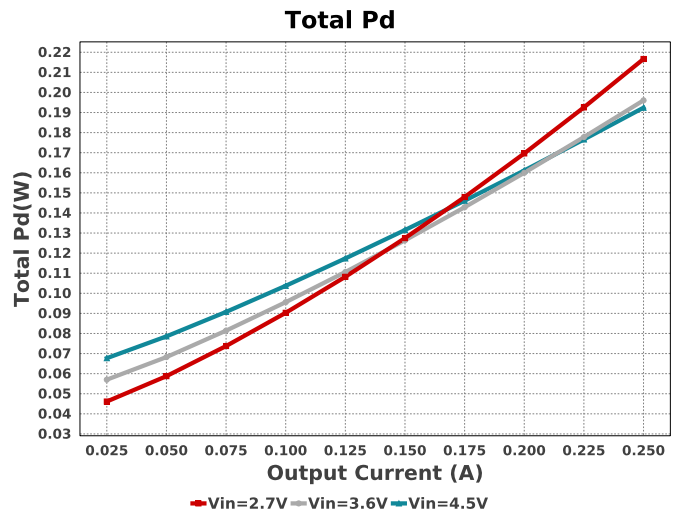
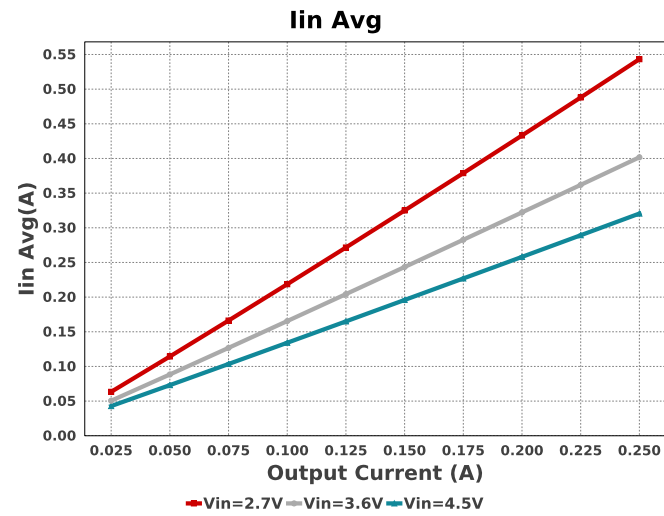
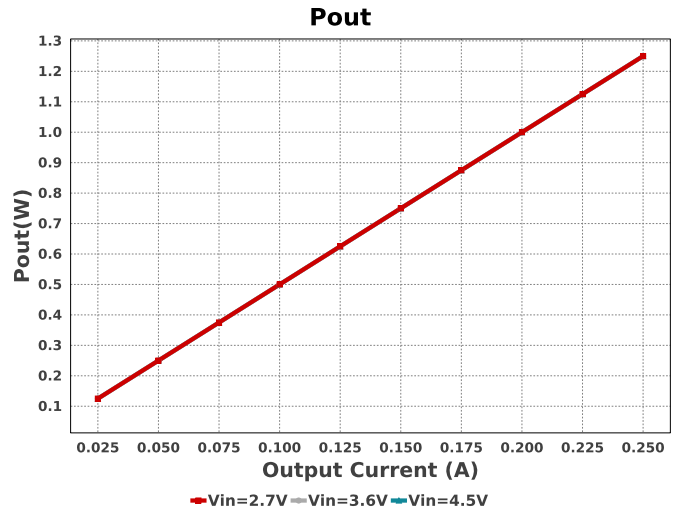
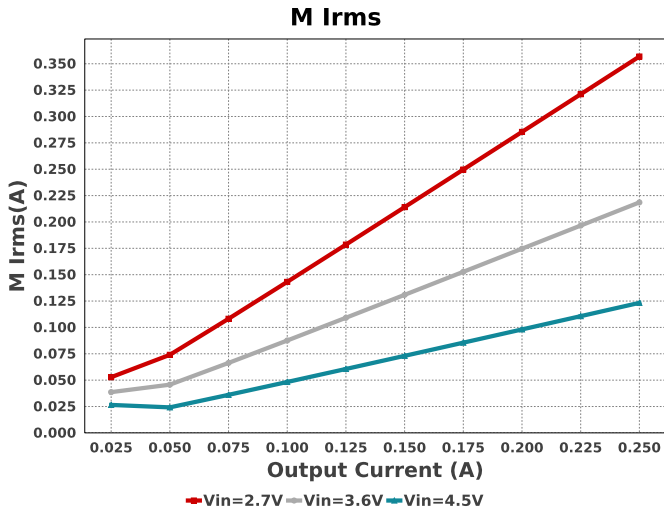
WEBENCH® Design Report

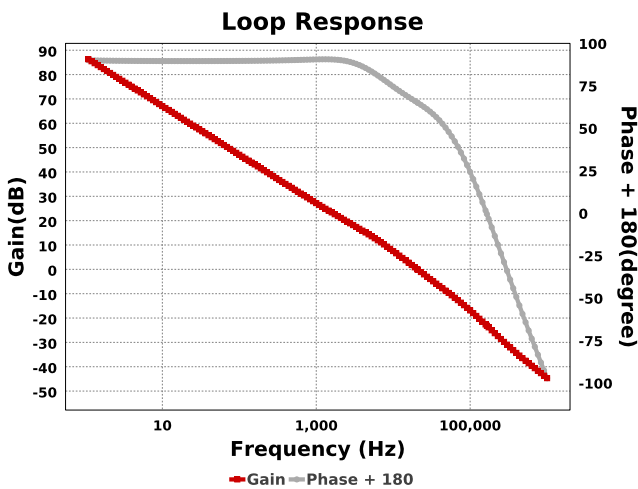
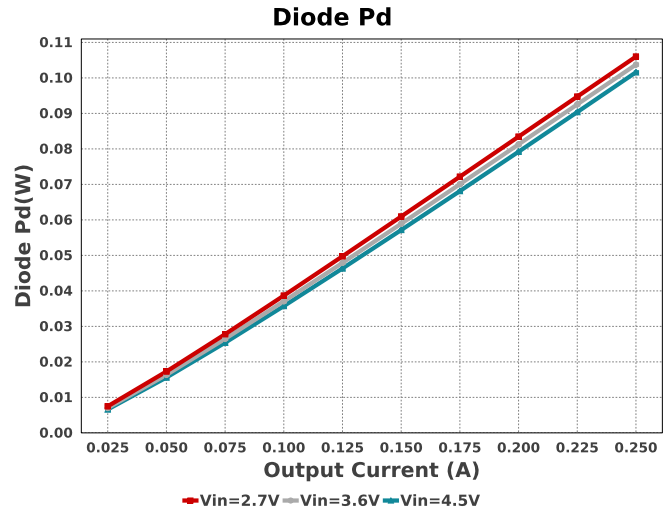
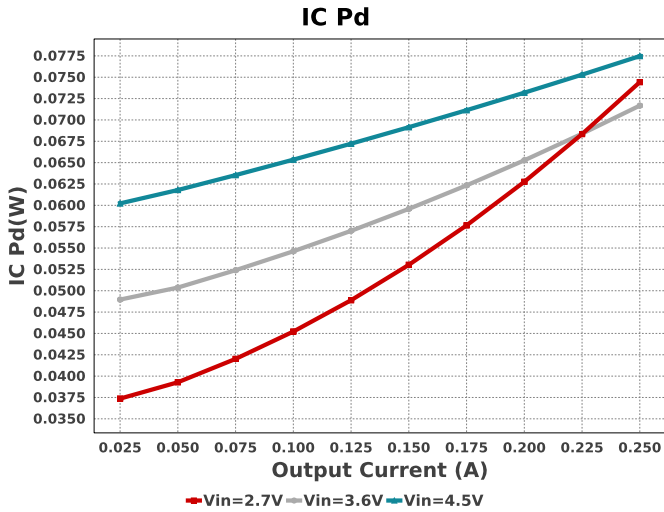
 Design : 83 LM2735XMF/NOPB
 LM2735XMF/NOPB 2.7V-4.2V to 5.00V @ 0.2A

Electrical BOM

| Name | Manufacturer | Part Number | Properties | Qty | Price | Footprint |
|---------|---------------------------|------------------------------------|---|-----|--------|-------------------------------|
| Cf | Samsung Electro-Mechanics | CL21C182JBF1PNE Series= C0G/NP0 | Cap= 1.8 nF VDC= 50.0 V IRMS= 0.0 A | 1 | \$0.02 | 0805 7 mm ² |
| Cin | Kemet | C0805C106K8PACTU Series= X5R | Cap= 10.0 uF ESR= 3.0 mOhm VDC= 10.0 V IRMS= 11.43 A | 1 | \$0.03 | 0805 7 mm ² |
| Cout | Kemet | C0805C106K8PACTU Series= X5R | Cap= 10.0 uF ESR= 3.0 mOhm VDC= 10.0 V IRMS= 11.43 A | 2 | \$0.03 | 0805 7 mm ² |
| D1 | Fairchild Semiconductor | SS14FL | VF@Io= 550.0 mV VRRM= 40.0 V | 1 | \$0.03 | SOD-123F 12 mm ² |
| L1 | NIC Components | NPI43C6R8MTRF | L= 6.8 uH 140.0 mOhm | 1 | \$0.11 | IND_NPI43C 31 mm ² |
| Renable | Yageo | RC0201FR-0710KL Series= ? | Res= 10.0 kOhm Power= 50.0 mW Tolerance= 1.0% | 1 | \$0.01 | 0201 2 mm ² |
| Rfbb | Yageo | RC0201FR-0710KL Series= ? | Res= 10.0 kOhm Power= 50.0 mW Tolerance= 1.0% | 1 | \$0.01 | 0201 2 mm ² |
| Rfbt | Yageo | RC0603FR-0730KL Series= ? | Res= 30.0 kOhm Power= 100.0 mW Tolerance= 1.0% | 1 | \$0.01 | 0603 5 mm ² |
| U1 | Texas Instruments | LM2735XMF/NOPB | Switcher | 1 | \$1.10 | MF05A 15 mm ² |









Operating Values

| # | Name | Value | Category | Description |
|-----|--------------|--------------|-----------|---|
| 1. | Cin IRMS | 36.906 mA | Capacitor | Input capacitor RMS ripple current |
| 2. | Cin Pd | 4.086 μW | Capacitor | Input capacitor power dissipation |
| 3. | Cout IRMS | 252.454 mA | Capacitor | Output capacitor RMS ripple current |
| 4. | Cout Pd | 95.6 μW | Capacitor | Output capacitor power dissipation |
| 5. | D1 Tj | 44.839 degC | Diode | D1 junction temperature |
| 6. | Diode Pd | 106.0 mW | Diode | Diode power dissipation |
| 7. | IC Ipk | 566.144 mA | IC | Peak switch current in IC |
| 8. | IC Pd | 74.426 mW | IC | IC power dissipation |
| 9. | IC Tj | 38.782 degC | IC | IC junction temperature |
| 10. | IC Tolerance | 25.0 mV | IC | IC Feedback Tolerance |
| 11. | ICThetaJA | 118.0 degC/W | IC | IC junction-to-ambient thermal resistance |
| 12. | Iin Avg | 543.2 mA | IC | Average input current |
| 13. | L Ipp | 127.85 mA | Inductor | Peak-to-peak inductor ripple current |
| 14. | L Pd | 35.502 mW | Inductor | Inductor power dissipation |
| 15. | M Iavg | 502.221 mA | Mosfet | MOSFET Average current |
| 16. | M Irms | 356.868 mA | Mosfet | MOSFET RMS ripple current |
| 17. | M Vds Act | 64.602 mV | Mosfet | Voltage drop across the MosFET |
| 18. | Cin Pd | 4.086 μW | Power | Input capacitor power dissipation |
| 19. | Cout Pd | 95.6 μW | Power | Output capacitor power dissipation |
| 20. | Diode Pd | 106.0 mW | Power | Diode power dissipation |
| 21. | IC Pd | 74.426 mW | Power | IC power dissipation |
| 22. | L Pd | 35.502 mW | Power | Inductor power dissipation |
| 23. | Total Pd | 216.652 mW | Power | Total Power Dissipation |
| 24. | BOM Count | 10 | System | Total Design BOM count |
| 25. | Cross Freq | 14.101 kHz | System | Bode plot crossover frequency |
| 26. | Duty Cycle | 50.221 % | System | Duty cycle |
| 27. | Efficiency | 85.228 % | System | Steady state efficiency |

| # | Name | Value | Category | Description |
|-----|----------------|----------------------|--------------------|--|
| 28. | FootPrint | 93.0 mm ² | System Information | Total Foot Print Area of BOM components |
| 29. | Frequency | 1.6 MHz | System Information | Switching frequency |
| 30. | Gain Marg | -19.23 dB | System Information | Bode Plot Gain Margin |
| 31. | Iout | 250.0 mA | System Information | Iout operating point |
| 32. | Low Freq Gain | 86.28 dB | System Information | Gain at 1Hz |
| 33. | Mode | CCM | System Information | Conduction Mode |
| 34. | Phase Marg | 61.464 deg | System Information | Bode Plot Phase Margin |
| 35. | Pout | 1.25 W | System Information | Total output power |
| 36. | Total BOM | \$1.38 | System Information | Total BOM Cost |
| 37. | Vin | 2.7 V | System Information | Vin operating point |
| 38. | Vout | 5.0 V | System Information | Operational Output Voltage |
| 39. | Vout Actual | 5.02 V | System Information | Vout Actual calculated based on selected voltage divider resistors |
| 40. | Vout Tolerance | 3.537 % | System Information | Vout Tolerance based on IC Tolerance (no load) and voltage divider resistors if applicable |
| 41. | Vout p-p | 7.978 mV | System Information | Peak-to-peak output ripple voltage |

Design Inputs

| Name | Value | Description |
|---------|---------|------------------------|
| Iout | 250.0 m | Maximum Output Current |
| VinMax | 4.5 | Maximum input voltage |
| VinMin | 2.7 | Minimum input voltage |
| Vout | 5.0 | Output Voltage |
| base_pn | LM2735X | Base Product Number |
| source | DC | Input Source Type |
| Ta | 30.0 | Ambient temperature |

WEBENCH® Assembly

Component Testing

Some published data on components in datasheets such as Capacitor ESR and Inductor DC resistance is based on conservative values that will guarantee that the components always exceed the specification. For design purposes it is usually better to work with typical values. Since this data is not always available it is a good practice to measure the Capacitance and ESR values of C_{in} and C_{out} , and the inductance and DC resistance of L1 before assembly of the board. Any large discrepancies in values should be electrically simulated in WEBENCH to check for instabilities and thermally simulated in WebTHERM to make sure critical temperatures are not exceeded.

Soldering Component to Board

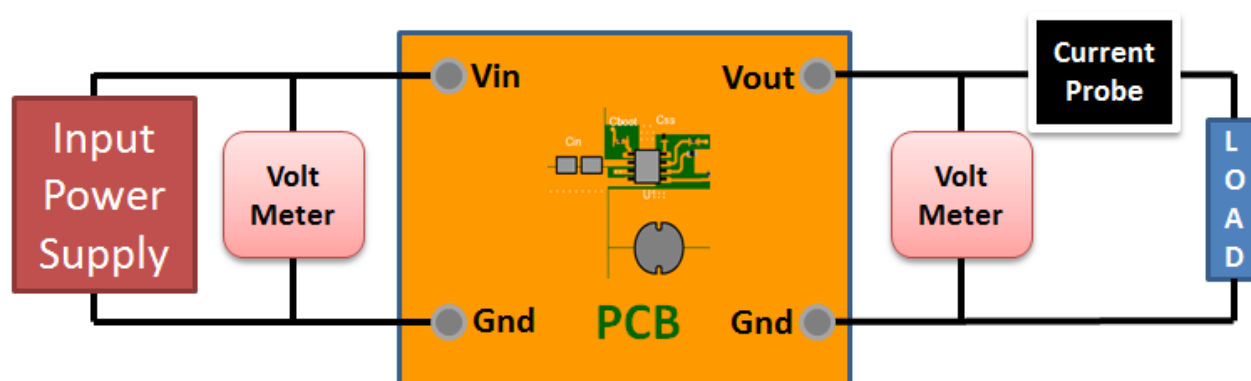
If board assembly is done in house it is best to tack down one terminal of a component on the board then solder the other terminal. For surface mount parts with large tabs, such as the DPAK, the tab on the back of the package should be pre-tinned with solder, then tacked into place by one of the pins. To solder the tab down to the board place the iron down on the board while resting against the tab, heating both surfaces simultaneously. Apply light pressure to the top of the plastic case until the solder flows around the part and the part is flush with the PCB. If the solder is not flowing around the board you may need a higher wattage iron (generally 25W to 30W is enough).

Initial Startup of Circuit

It is best to initially power up the board by setting the input supply voltage to the lowest operating input voltage 2.7V and set the input supply's current limit to zero. With the input supply off connect up the input supply to V_{in} and GND. Connect a digital volt meter and a load if needed to set the minimum load of the design from V_{out} and GND. Turn on the input supply and slowly turn up the current limit on the input supply. If the voltage starts to rise on the input supply continue increasing the input supply current limit while watching the output voltage. If the current increases on the input supply, but the voltage remains near zero, then there may be a short or a component misplaced on the board. Power down the board and visually inspect for solder bridges and recheck the diode and capacitor polarities. Once the power supply circuit is operational then more extensive testing may include full load testing, transient load and line tests to compare with simulation results.

Load Testing

The setup is the same as the initial startup, except that an additional digital voltmeter is connected between V_{in} and GND, a load is connected between V_{out} and GND and a current meter is connected in series between V_{out} and the load. The load must be able to handle at least rated output power + 50% (7.5 watts for this design). Ideally the load is supplied in the form of a variable load test unit. It can also be done in the form of suitably large power resistors. When using an oscilloscope to measure waveforms on the prototype board, the ground leads of the oscilloscope probes should be as short as possible and the area of the loop formed by the ground lead should be kept to a minimum. This will help reduce ground lead inductance and eliminate EMI noise that is not actually present in the circuit.



Design Assistance

1. Master key : F1A72540DE348381[v1]
2. **LM2735X** Product Folder : <http://www.ti.com/product/LM2735> : contains the data sheet and other resources.

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